

## LETTER TO THE EDITOR

Discussion of "Torsional vibrations of a circular disk on an infinite transversely isotropic medium", *Int. J. Solids Structures*, Vol. 25, No. 9, pp. 1069-1076 (1989)

In a recent article, Tsai (1989) presented an analytical formulation for the mixed boundary value problem related to time-harmonic torsional vibrations of a circular rigid disk bonded to the surface of a transversely isotropic elastic half space. Numerical solutions for the compliance function, contact shear stress and resonant amplitudes were also presented. The study by Tsai (1989) is a welcome addition to the literature on contact problems and the numerical results are useful to engineering practice. A review of the solution procedure, however, indicates that the solution for the problem can be obtained from the solution for the isotropic case (Reissner and Sagoci, 1944; Gladwell, 1969; Keer *et al.*, 1974; Luco, 1976) through the use of a scalar transformation. Therefore, a complete analysis is unnecessary. The following presents the proof of this statement and it is shown that similar correspondence exists, even in the case of a transversely isotropic elastic layer.

Consider the axisymmetric torsional vibration of a transversely isotropic elastic half space. A cylindrical coordinate system  $(r, \theta, z)$  is employed in the analysis with the  $z$ -axis parallel to the material axis of symmetry. The entire problem, including the coordinate frame, is nondimensionalized with respect to the radius  $a$  of the disk. The nonzero stress components  $\sigma_{r\theta}$  and  $\sigma_{z\theta}$  can be expressed in terms of the displacement  $v$  in the  $\theta$ -direction, as:

$$\sigma_{r\theta} = \frac{(c_{11} - c_{12})}{2} \left( \frac{\partial v}{\partial r} - \frac{v}{r} \right) \quad (1a)$$

$$\sigma_{z\theta} = c_{44} \frac{\partial v}{\partial z}, \quad (1b)$$

where  $c_{11}$ ,  $c_{12}$  and  $c_{44}$  are material constants (Lekhnitskii, 1963).

The displacement  $v$  is governed by

$$\frac{(c_{11} - c_{12})}{2} \left[ \frac{\partial^2 v}{\partial r^2} + \frac{1}{r} \frac{\partial v}{\partial r} - \frac{v}{r^2} \right] + c_{44} \frac{\partial^2 v}{\partial z^2} = \rho \frac{\partial^2 v}{\partial t^2}, \quad (2)$$

where  $\rho$  is the density of the medium.

It is assumed that the motion is time-harmonic with circular frequency  $\omega$ . A solution of eqn (2) can be expressed as:

$$v(r, z) = \int_0^\infty [A(\xi) e^{-\beta z} + B(\xi) e^{\beta z}] J_1(\xi r) d\xi, \quad (3)$$

where

$$\beta^2 = \xi^2 - k^2; \quad \bar{z} = z/\gamma; \quad \gamma = \left( \frac{2c_{44}}{c_{11} - c_{12}} \right)^{1/2}; \quad k^2 = \frac{\rho \omega^2 \gamma^2}{c_{44}}$$

and  $J_1$  is the Bessel function of the first kind and first order.

In view of eqns (1) and (3), the shear stress  $\sigma_{z\theta}$  can be expressed as :

$$\sigma_{z\theta}(r, z) = \frac{c_{44}}{\gamma} \int_0^{\infty} \beta [-A(\xi) e^{-\beta z} + B(\xi) e^{\beta z}] J_1(\xi r) d\xi. \quad (4)$$

The boundary value problem related to torsional vibration of the rigid disk can be expressed as :

$$v(r, 0) = \phi_0 r, \quad 0 \leq r < 1 \quad (5a)$$

$$\sigma_{z\theta}(r, 0) = 0, \quad r > 1 \quad (5b)$$

where  $\phi_0$  is the rotation of the disk about the  $z$ -axis.

Substitution of eqns (3) and (4) into eqn (5), together with the condition that  $B(\xi) \equiv 0$  for an elastic half space region ( $0 \leq z < \infty$ ), yields the following dual integral equation system for  $A(\xi)$  :

$$\int_0^{\infty} A(\xi) J_1(\xi r) d\xi = \phi_0 r \quad 0 \leq r < 1; \quad (6a)$$

$$\int_0^{\infty} \beta A(\xi) J_1(\xi r) d\xi = 0 \quad r > 1. \quad (6b)$$

The torque  $T_0$  acting on the disk can be expressed as :

$$T_0 = -\frac{2\pi c_{44} a^3}{\gamma} \int_0^1 r^2 \left[ \int_0^{\infty} \beta A(\xi) J_1(\xi r) d\xi \right] dr. \quad (7)$$

Now, consider an identical boundary value problem for an isotropic half space with shear modulus  $c_{44}$  and mass density  $\rho$ . Let  $\bar{\omega}$  denote the circular frequency in this case ; the corresponding general solution for displacement  $\bar{v}$  can be expressed as :

$$\bar{v}(r, z) = \int_0^{\infty} [\bar{A}(\xi) e^{-\beta z} + \bar{B}(\xi) e^{\beta z}] J_1(\xi r) d\xi, \quad (8)$$

where

$$\bar{\beta}^2 = \xi^2 - \bar{k}^2 \quad \text{and} \quad \bar{k}^2 = \frac{\rho \bar{\omega}^2}{c_{44}}.$$

The boundary value problem is governed by

$$\int_0^{\infty} \bar{A}(\xi) J_1(\xi r) d\xi = \phi_0 r, \quad 0 \leq r < 1; \quad (9a)$$

$$\int_0^{\infty} \bar{\beta} \bar{A}(\xi) J_1(\xi r) d\xi = 0, \quad r > 1. \quad (9b)$$

The torque  $\bar{T}_0$  acting on the disk can be expressed as :

$$\bar{T}_0 = -2\pi c_{44} a^3 \int_0^1 r^2 \left[ \int_0^\infty \bar{\beta} \bar{A}(\xi) J_1(\xi r) d\xi \right] dr. \quad (10)$$

It is noted that if  $\bar{k} = k$  then  $\beta = \bar{\beta}$  and comparison of eqns (6) and (9) yields  $\bar{A}(\xi) = A(\xi)$ . In addition, comparison of eqns (7) and (10) yields  $T_0 = \bar{T}_0/\gamma$ . The condition  $\bar{k} = k$  implies that  $\bar{\omega} = \omega\gamma$ . Therefore, the torque  $T_0$  at frequency  $\omega$  corresponding to the transversely isotropic problem is equal to  $1/\gamma$  times the torque corresponding to the isotropic problem at frequency  $\omega\gamma$ . An identical relation exists between the shear stress  $\sigma_{\theta z}$ .

Next, consider the case of a rigid circular disk bonded to a transversely isotropic elastic layer of nondimensional thickness  $h$ , overlying a rigid base. In this case,  $B(\xi) \neq 0$  in eqn (3). The boundary value problem is defined by eqns (5) together with the condition

$$v(r, h) = 0 \quad (11)$$

Equation (11) implies that

$$B(\xi) = -A(\xi) e^{-2\beta h^*}, \quad (12)$$

where  $h^* = h/\gamma$ .

The boundary value problem is governed by

$$\int_0^\infty A(\xi) [1 - e^{-2\beta h^*}] J_1(\xi r) d\xi = \phi_0 r, \quad 0 \leq r < 1; \quad (13a)$$

$$\int_0^\infty \beta A(\xi) [-1 + e^{-2\beta h^*}] J_1(\xi r) d\xi = 0, \quad r > 1. \quad (13b)$$

An identical problem for an isotropic layer of nondimensional thickness  $\bar{h}$  is governed by

$$\int_0^\infty \bar{A}(\xi) [1 - e^{-2\beta \bar{h}}] J_1(\xi r) d\xi = \phi_0 r \quad (14a)$$

$$\int_0^\infty \bar{\beta} \bar{A}(\xi) [-1 + e^{-2\beta \bar{h}}] J_1(\xi r) d\xi = 0. \quad (14b)$$

It is evident from eqns (13) and (14) that if  $\beta = \bar{\beta}$  and  $h^* = \bar{h}$ , then  $A(\xi) = \bar{A}(\xi)$ .

Therefore, the torque corresponding to a transversely isotropic layer of height  $h$  at frequency  $\omega$  is equal to  $1/\gamma$  times the torque corresponding to an isotropic layer of thickness  $h/\gamma$  at frequency  $\omega\gamma$ . A similar correspondence exists between the stress  $\sigma_{z\theta}$ . Numerical solutions for the isotropic elastic layer problem are given by Gladwell (1969) and Keer *et al.* (1974).

It is noted that the above type of direct correspondence between isotropic and transversely isotropic material exists only for a *limited class of problems involving axisymmetric torsional deformations*. In the case of general deformations, a formal solution is required. A recent article by Wang and Rajapakse (1990) considers general asymmetric boundary value problems related to a transversely isotropic medium under static loading, and elastodynamic problems (Rajapakse and Wang, 1991) are also currently under study.

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